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## Linear-brightness controller for LEDs has 64 taps

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Applications that include LEDs but no microcontroller or other form of control intelligence can benefit from a simple circuit that provides manual control of the LEDs' light intensity. Among the devices suitable for this purpose are mechanical (analog) and electronic (digital) potentiometers. The digital potentiometer with up and down pushbuttons, an alternative to the mechanical potentiometer, is smaller, more reliable, and usually less expensive (Figure 1).

IC<sub>2</sub>, a current regulator, drives a chain of LEDs with current as high as 200 mA. In a standard application circuit, IC<sub>2</sub>'s internal regulator senses the drop across current-sense resistor R<sub>SENSE</sub> in series with the LED chain. Thus, IC<sub>2</sub> controls current through the chain by regulating voltage at the differential inputs, CS<sup>-</sup> and CS<sup>+</sup>, to the set value of 204 mV. Resistors R<sub>A</sub> and R<sub>B</sub> allow the output voltage IC<sub>1</sub>'s Pin 6 to adjust the current level. IC<sub>1</sub> is a 64-tap linear digital potentiometer whose resistance connects between ground and V<sub>5</sub>, a well-regulated voltage that IC<sub>2</sub> internally generates. You manually adjust the RW control voltage (Pin 6), a fraction of V<sub>5</sub>, using the up and down pushbuttons. A few assumptions allow a quick and simplified calculation of the neces-

sary resistor values. Initially, you fix R<sub>A</sub> and then calculate R<sub>B</sub> and R<sub>SENSE</sub>. The assumptions are that you can neglect the maximum 6.93-μA error induced by the bias current at CS<sup>+</sup>; that the value you choose for R<sub>A</sub> is much higher than IC<sub>1</sub>'s equivalent resistance, for which the worst-case value at position 32 (top and bottom resistances plus the wiper series resistance) is 2.9 kΩ; and that R<sub>SENSE</sub> is much less than R<sub>B</sub>.

After setting R<sub>A</sub> at 25.5 kΩ,  $V_{WIPER} = (5V/63) \times N$ , where N is the wiper setting (0 to 63). Then, you solve the equation  $(V_{WIPER} - 0.204V) / R_A = (0.204V - I_{LED} \times R_{SENSE}) / R_B$ . Solve the above equation for R<sub>B</sub> under the conditions for which I<sub>LED</sub> = 0, which are N = 63 and V<sub>WIPER</sub> = 5V (top position):  $R_B = 25.5 \text{ k}\Omega \times 0.204V / (5V \times 0.204V) = 1.085 \text{ k}\Omega$ . You can choose R<sub>B</sub> from the standard values of 1.07 kΩ (1% series)

### DIs Inside

72 Controlled power supply increases op amps' output-voltage range

76 Single-IC-based electronic circuit replaces mechanical switch

78 Microcontroller drives H bridge to power a permanent-magnet dc motor

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or 1.1 kΩ (5% series). At the bottom position, where V<sub>WIPER</sub> = 0 and LED current is the maximum of 200 mA, brightness should be the maximum available. Solving for R<sub>SENSE</sub>,  $R_{SENSE} = [0.204V + (0.204V \times (1.085 / 25.5))] / 0.2A = 1.063\Omega$ ; 1.07Ω is a standard value in the 1% series.

A graph of LED current versus tap position shows a slight nonlinearity

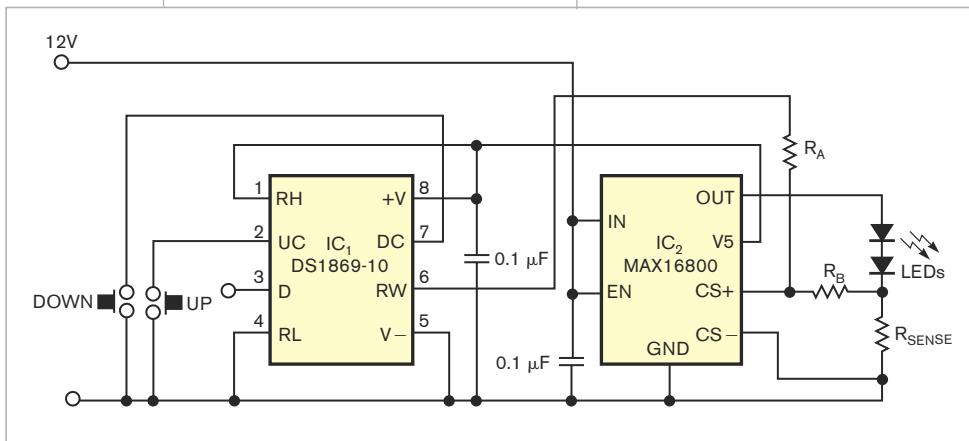
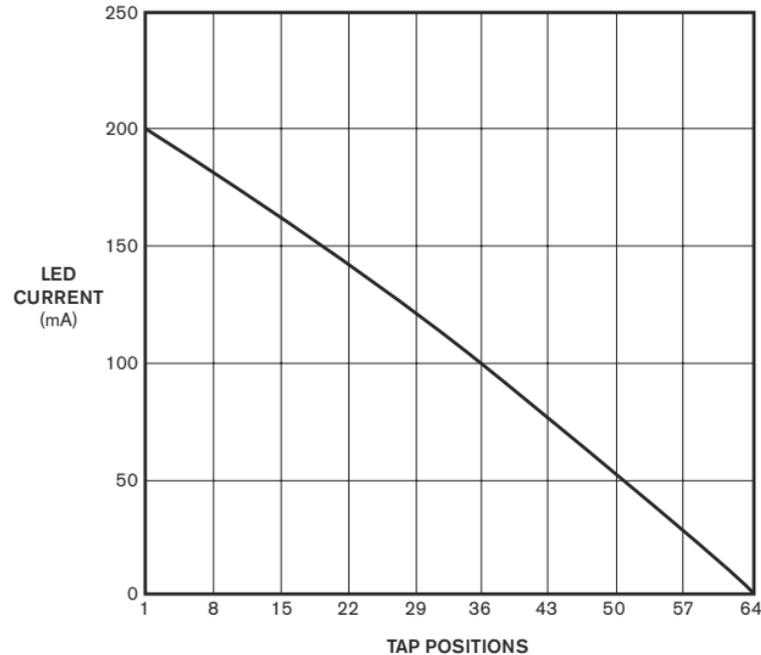


Figure 1 This brightness-control circuit lets you manually adjust the LED brightness using the up and down buttons.

because of the variation in resistance you see looking into the wiper at different tap positions (**Figure 2**). At the extreme ends of the potentiometer, you see only the  $400\Omega$  wiper resistance. As the wiper moves toward midpoint, the resistance increases toward a maximum of one-quarter of the end-to-end resistance value. Because  $IC_1$  is a  $10\text{-k}\Omega$  potentiometer, the resistance the wiper sees at midpoint is about  $2.5\text{ k}\Omega$  in series with  $R_{\text{WIPER}}$ . This variation introduces a maximum linearity error of 8%, which is negligible in most LED applications.  $IC_2$  offers thermal protection against excessive heat and overload conditions. For effective power dissipation and to avoid thermal cycling, you must connect the exposed pad of the package to a large-area ground plane. **EDN**



**Figure 2** A plot of LED current versus tap position in Figure 1 exhibits only a slight nonlinearity.