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Astable multivibrator lights LED from a single cell

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Lighting LEDs from a single 1.5V cell poses a problem because their forward voltages are higher than the cell's. The simplest way to light the LED is to use a step-up dc/dc converter. This Design Idea offers a simple and reliable alternative for applications in which low cost is of primary concern. The circuit in Figure 1 employs a classic astable oscillator, which transistors Q₁ and Q₂ form. The square-wave drive signal at Q₂'s collector turns a PNP switching transistor, Q₃, on and off. When Q₃ turns on, it charges inductor L₁, and, when it turns off, inductor L₁ discharges its stored energy through the LED during flyback, allowing you to light any type or color of LED.

The astable circuit oscillates at a frequency of 1/T_O, where T_O = T_L + T_H with T_L ≈ 0.76R₂C₂ and T_H ≈ 0.76R₁C₁ when the cell voltage is 1.5V, where T_O is the time, T_L is the on-time, and

T_H is the off-time. With the component values in Figure 1, the frequency and the duty cycle are about 28.5 kHz and 50%, respectively. During the on-time, transistor Q₃ is on, and inductor L₁ starts to charge with constant voltage so its current ramps up linearly to a peak value, as the following equation describes: $I_{L_{PEAK}} = [(V_{BAT} - V_{CESATQ3}) / L_1] \times T_L$, where I_{L_{PEAK}} is the peak current of L₁, V_{BAT} is the battery voltage, and V_{CESATQ3} is the collector-to-emitter saturation voltage of Q₃. During the off-time, Q₃ is off, and the inductor's voltage reverses polarity, forward-biasing the LED and discharging through it at a constant voltage roughly equal to the forward voltage of the LED while its current ramps down to zero.

Because this cycle repeats at a high rate, the LED appears always on. The LED's brightness depends on its own average current, which is proportional to the peak value. Because the LED

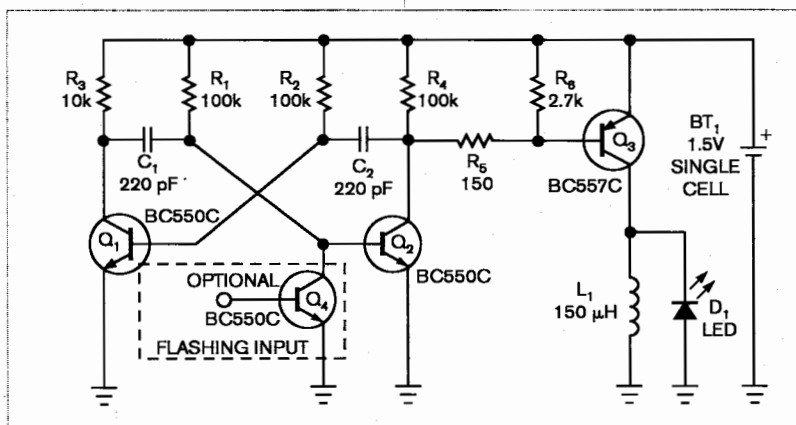
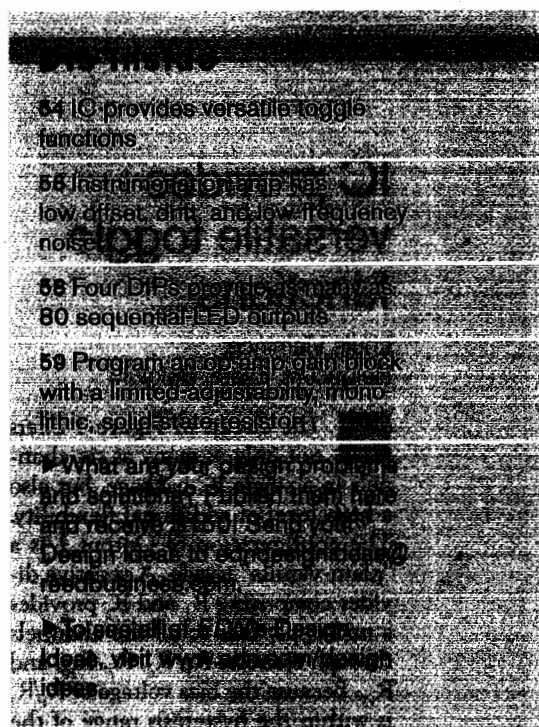


Figure 1 This simple astable multivibrator provides a low-cost way to drive an LED from a single cell.

current is roughly a triangular pulse with a peak current approximately equal to the inductor's current because of the finite turn-off time of Q₃, you can easily estimate the average current: $I_{LED_{AVG}} \approx (\frac{1}{2}) \times I_{L_{PEAK}} \times (T_{DIS} / T_O)$, where T_{DIS} is the discharge time of inductor L₁ through the LED, which you can roughly estimate from the slope of L₁'s discharge, which is V_{LED}/L₁, where V_{LED} is the LED's voltage.

To control the LED's brightness, you may increase or decrease the inductor's peak current by varying its inductance from 100 to 330 μH to achieve the optimal brightness for the type of LED you are using. However, L₁'s charge slope is always smaller than its discharge slope, and, because T_L and T_H are equal, L₁ has enough time to discharge completely. When it recharges on its next cycle, its current

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cycle always starts from zero. If this is not the case—if you reduce T_H too much, for example—the inductor current increases on each cycle until Q_3 goes out of saturation, and the final current value becomes unpredictable because it depends on Q_3 's dc gain. Optional transistor Q_4 allows the circuit to flash the LED when a low-fre-

quency gating signal drives its base.

No one component is critical; for example, any small-signal transistor is suitable. But, if possible, choose a PNP transistor for Q_3 with high dc-current gain and low collector-to-emitter saturation voltage for best efficiency. Also, take care that the peak current does not saturate L_1 and does not exceed the

maximum peak-current rating of Q_3 and the LED. The astable circuit starts to operate with a supply voltage as low as 0.6V, but the LED is off and begins to light dimly when the supply voltage exceeds 0.9V. When the supply voltage exceeds 1V, the LED's brightness is adequate, even if it depends slightly on the forward voltage of the LED. **EDN**